Table 1. The Berea sandstone core properties

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|--|--------------|----------------|--------|--------|-------|---------|----------------------------|--|--|
| Core # | D, cm | L, cm | Kg, md | φ, % | Swi,% | μ₀, ср | Wetness | | |
| Soltrol 220, no aging VSWW | | | | | | | | | |
| Ev8h8b | 3.764 | 7.91 | 73.9 | 0.1615 | 22.6 | 3:8 | VSWW | | |
| Ev8h9a | 3.739 | 8.057 | 82.9 | 0.1601 | 20.9 | 3.8 | | | |
| Ev8h9b | 3.742 | 7.922 | 76.7 | 0.1588 | 24.6 | 3.8 | VSWW | | |
| Ev8h10a | 3.761 | 8.047 | 76.7 | 0.1636 | 22.7 | 3.8 | VSWW | | |
| Ev8h10b | 3.764 | 7.83 | 70.1 | 0.1627 | 22.5 | 3.8 | VSWW | | |
| Ev8h17a | 3.763 | 8.245 | 77.4 | 0.1734 | 22.59 | 3.8 | VSWW | | |
| Ev8h18a | 3.753 | 7.894 | 95.8 | 0.1746 | 23.02 | 3.8 | VSWW | | |
| Minnelusa 2002 crude oil | | | | | | | | | |
| Ev8hla | 7.864 | 3.786 | 101.5 | 0.1760 | 23.9 | 68.0 | MXW, 10d aging | | |
| Ev8h2b | 7.538 | 3.765 | 71.7 | 0.1652 | 23.7 | 68.0 | MXW, 10d aging | | |
| Ev8h3a | 3.764 | 7.963 | 70.1 | 0.1678 | 24.3 | 1.5 | MXW-F (Dakota), 10d aging | | |
| Ev8h4a | 3.764 | 8.06 | 65.1 | 0.1636 | 24.3 | 68.0 | MXW, 10d aging | | |
| Ev8h4b | 7.680 | 3.767 | 66.6 | 0.1628 | 24.6 | 680 | MXW, Id aging | | |
| Ev8h5a | 8.242 | 3.764 | 68.2 | 0.1649 | 24.6 | 68.0 | MXW, no aging | | |
| Ev8h5b | 3.766 | 7.754 | 74.6 | 0.1664 | 24.4 | 3.8 | MXW-F (S220), no aging | | |
| Ev8h6b | 7.736 | 3.764 | 67.6 | 0.1605 | 22.0 | 68.0 | MXW, 10d aging | | |
| Ev8h7b | 3.765 | 7.67 | 72.4 | 0.1603 | 22.5 | 1.5 | MXW-F (Dakota), no aging | | |
| | 3.758 | 7.791 | 120 | 0.1743 | 22.8 | 1.5 | MXW (Dakota), no aging | | |
| Ev8h11b | 3.758 | 8.105 | 126.2 | 0.1754 | 23.2 | 68.0 | MXW, no aging | | |
| Ev8h13a | 8.280 | 3.759 | 114.0 | 0.1778 | 22.1 | 68.0 | MXW, 10d aging | | |
| Ev8h16a | 3.76 | 7.921 | 117.2 | 0.1774 | 21.3 | 68.0 | MXW, 10d aging | | |
| Ev8h16b | | 8.262 | 133.1 | 0.1749 | 18.8 | 68.0 | MXW, 4d aging, 45°C | | |
| Ev8h29a | 3.75 | 3.788 | 58.2 | 0.1748 | 23.3 | 68.0 | MXW, 10d aging | | |
| Ev7v1b | 7.644 | 7.581 | 46.2 | 0.1703 | 22.0 | 68.0 | MXW, 10d aging | | |
| Evlvld | 3.777 | | 113 | 0.1703 | 23.9 | 68.0 | MXW, 10d aging | | |
| Ev5hlc | 3.787 | 7.634 | 113 | 0.162 | 23.5 | | | | |
| | 5 cruide oil | 7.025 | 119.3 | 0.1731 | 21.3 | 19.2 | MXW, 10d aging | | |
| Ev8h13b | 3.758 | 7.835 8.076 | 109.6 | 0.1717 | 22.6 | 19.2 | . MXW, no aging | | |
| Ev8h14a | 3.759 | | 106.2 | 0.1708 | 22.0 | 1.5 | MXW-F (Dakota), no aging | | |
| Ev8h14b | 3.76 | 7.839 | | 0.1778 | 22.2 | 1.5 | MXW-F (Dakota), no aging | | |
| Ev8h15a | 3.757 | 8.228 | 111.1 | 0.1776 | 22.7 | 19.2 | MXW, no aging | | |
| Ev8h15b | 3.759 | 7.974 | 87.6 | 0.1770 | 22.6 | 33.9 | MXW-F (frontier), no aging | | |
| Ev8h21b | 3.758 | 7.686 | 87.0 | 0.174 | 22.0 | 1 ,55.5 | | | |
| | Draw crude | 011 | 700 | 0.1698 | 23.1 | 3.8 | MXW-F (S220), no aging | | |
| Ev8hl9a | 3_756 | 7.866 | 70.9 | | 23.3 | 7.0 | MXW, no aging | | |
| Ev8h21a | 3_758 | 7.832 | 84.8 | 0.1724 | | 7.0 | MXW, no aging | | |
| Ev8h27b | 3.750 | 7.758 | 119.7 | 0.1741 | 23.6 | 7.0 | MXW, 10d aging | | |
| Ev8h28b | 3_750 | 8.056 | 121.2 | 0.1794 | 22.3 | 7.0 | MXW, 2d aging | | |
| Ev8h30a | 3_748 | 7.597 | 86.8 | 0.1705 | <24.7 | 7.0 | MXW. 2d aging | | |
| Ev8h30b | 3.752 | 7.153 | 86 | 0.1717 | <26.3 | 7.0 | | | |

Table 2. The Limestone core properties

| Table 2. The Elinestone core properties | | | | | | | | | | |
|---|--------------|-------|---------------------|--------|-------|---------------------|--|--|--|--|
| Core # | D, cm | L, cm | K _g , md | φ, % | Swi,% | μ ₀ , cp | Wetness | | | |
| Oil recovery (Cottonwood oil) | | | | | | | | | | |
| 1TC15a | 3.724 | 7.477 | 19.1 | 0.2696 | 24.3 | 24.1 | MXW, 10d aging | | | |
| T2Tc11a | 3.729 | 7.320 | .14.7 | 0.2767 | 18.59 | 24.1 | MXW, 10d aging | | | |
| T2Tc21a | 3.698 | 7.797 | 7.1 | 0.2300 | 22.12 | 24.1 | MXW, 10d aging | | | |
| Gas flood | Gas flooding | | | | | | | | | |
| 1TC8b | 3.734 | 6.59 | 3.7 | 18.0 | 100 | | VSWW | | | |
| 1TC20b | 3.749 | 7.452 | 6.1 | 21.6 | 100 | | VSWW | | | |
| 1TC24b | 3.753 | 7,593 | 3.6 | 18.0 | 100 | | VSWW | | | |
| 3TC18b | 3.740 | 6.490 | 1.4 | 20.2 | 21.4 | | VSWW | | | |
| 2TC4b | 3.788 | 6.481 | 3.4 | · 22.8 | 21.7 | | Tensleep/S130, 2d aging | | | |
| 1TC24b | 3.753 | 7.593 | 3.6 | 18.0 | 27.5 | | BS oil (the 2 nd and 3 rd cycle), 2d aging | | | |

Table 3. Selected properties of crude and refined oils

| | Oils | ρ, g/mL @20°C | η, cP @~22°C | IFT, mN/M @20°C | Asphalt.% |
|-------------------|----------------|------------------|-----------------|--------------------|-----------|
| | Minnelusa 2002 | 0.9076 | 68 | 23.4 | 9.5 |
| Asphaltic | Black Mt. | 0.9219 | 134 | | 8.1 |
| crudes | Tensleep 95 | 0.8692 | 19.2 | 23.3 | 3.2 |
| · | Cottonwood | 0.8874 | 24.1 | 28.9 | 2.3 |
| | Big Sand Draw | 0.8496 | 7.0 | 21.5 | 1.6 |
| Mineral oils | S220 | 0.7869 | 3.8 | 49.5 | 0 |
| | S130 , | 0.7605 | 1.6 | ~50 | ´0 |
| | Pentane | | | ~50 | 0 |
| | Dakota | 0.7741 | 1.5 | 34.2 | 0 |
| Paraffinic crudes | Frontier | 0.8338 | 21.8 | 33.8 | . 0 |

Table 4 Synthetic brine composition

| | Table 4. Symmetic composition | | | | | | | |
|---|-------------------------------|---------------|--------------|----------------------------|----------------------------|---------------------------|-----|---------------|
| | Brine | NaCl (g/L) | KCI (g/L) | CaCl ₂ (g/L) | MgCl ₂ (g/L) | NaN ₃ (g/L) | рН | TDS (mg/L) |
| | | | | | | | - | 26770 |
| - | Sea water | 28 | 0.935 | 2.379 | 5.365 | 0.1 | 6.6 | 36779 |

Table 5 Interfacial tensions (Aqueous phase = SSW)

| Oleic phase | IFT, mN/m | Temp.,°C |
|---------------------------|-----------|----------|
| S220 | 49.5 | 20.0 |
| S220 | 1.7 | 20.0 |
| S220+0.025%polyamine | 24.3 | 20.0 |
| S220+0.2%RAP | 0.03 | 20.0 |
| S220+O.05%RAP | 0.55 | 20.0 |
| S220+O.025%PA+0.05%RAP | 1.0 | 20.0 |
| S220+O.2%TDA-6 | 1.34 | 20.0 |
| S220+O.1%DA-4 | 11.7 | 20.0 |
| S220+O.1%oleic acid | 29.8 | 20.0 |
| Minnelusa 2002 crude oil | 23.4 | 20.0 |
| Dakota crude oil | 34.2 | 20.0 |
| Tensleep 1995 crude oil | 23.3 | 20.0 |
| Big SarıdDraw crude oil | 21.5 | 20.0 |
| Frontier crude oil | 33.8 | 20.0 |
| M'02+0.025%PA | 17.7 | 20.0 |
| M'02+O.05%RAP | 8.6 | 20.0 |
| Dakota oil+0.025%PA | 7.9 | 20.0 |
| Tensleep 95 +0.05%PA | 10.5 | 20.0 |
| BS oil +0.05%PA | 10 | 20.0 |
| BS oil + 0.1%PA | 7.2 | 20.0 |
| BS oil + 0.1%PA | 4.3 | 75.0 |
| Cottonwood oil +0.025% PA | 12.1 | 20.0 |
| Cottonwood oil | 28.9 | 20.0 |

Table 6 Asphaltene precipitation

| 1 | Minnelusa crude | Black Mountain crude | Tensleep crude | Big Sand Draw |
|--------------|--------------------|------------------------|-------------------|------------------|
| S220 or S130 | Yes | Yes | Yes | Yes |
| Dakota oil | Yes | Yes | Yes | Yes |
| Frontier oil | | Yes (under microscope) | No | No |

Fig. 1 Method 1 of treatment for oil reservoir case

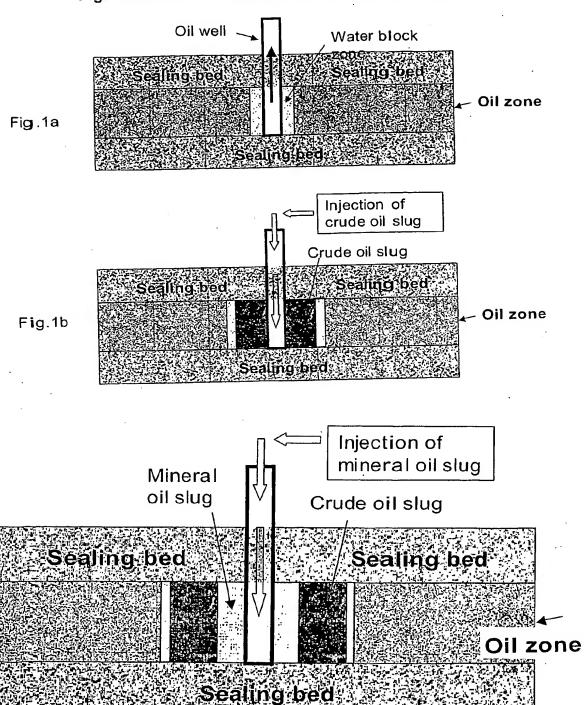


Fig.1c

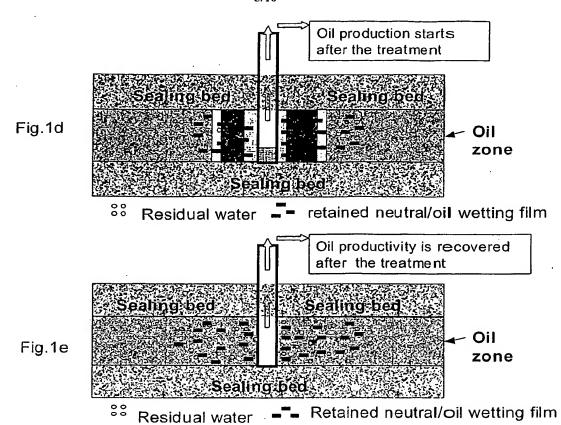


Fig. 2 The sketch of water saturation change near well bore vs. cycle numbers of treatment

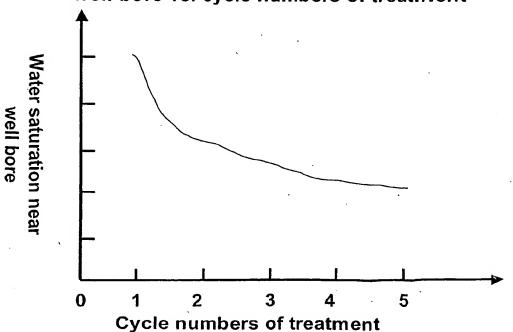


Fig. 3 Method 2 of treatment for oil reservoir case

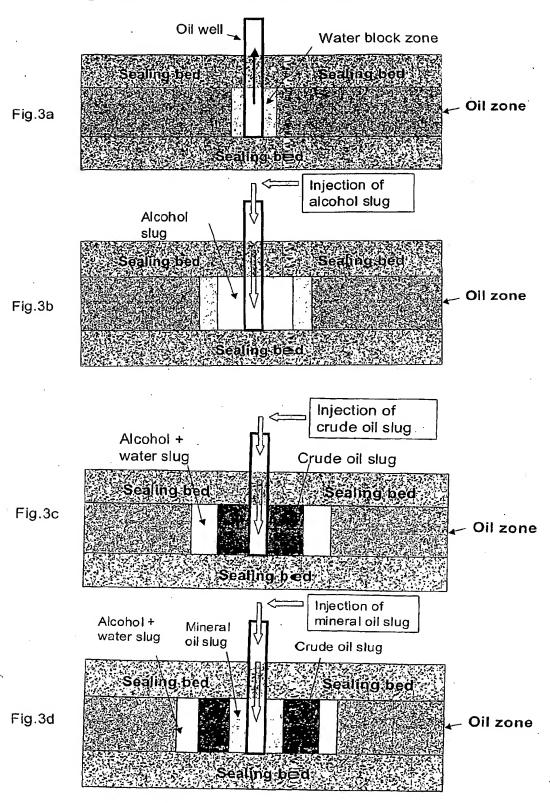
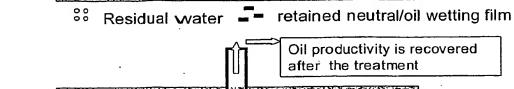
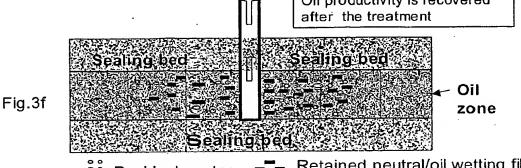


Fig.3e

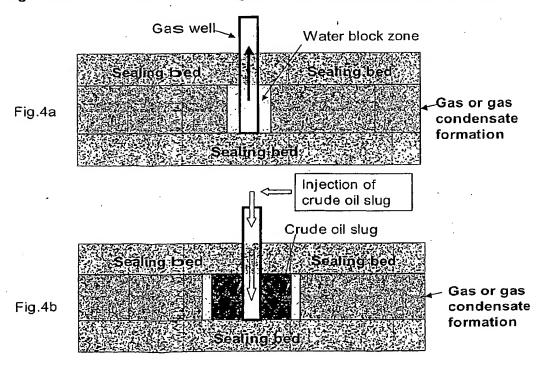
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Retained neutral/oil wetting film Residual water

Fig. 4 Method 1 of treatment for gas or gas condensate reservoir case



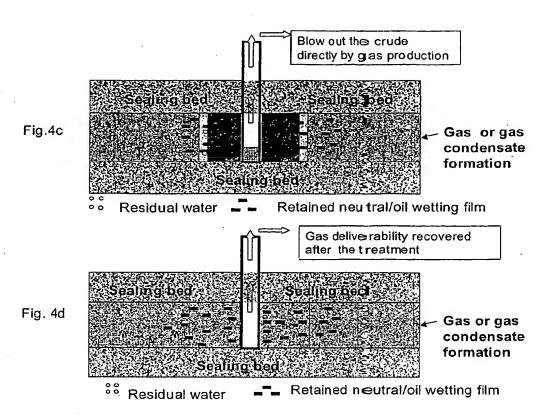
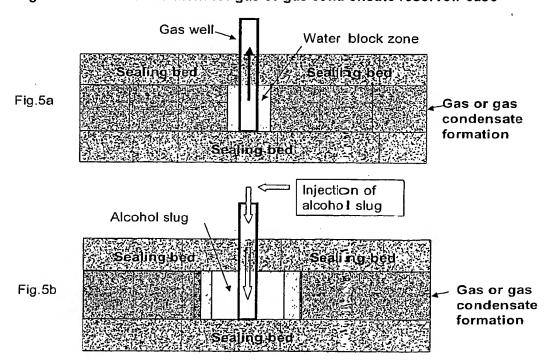
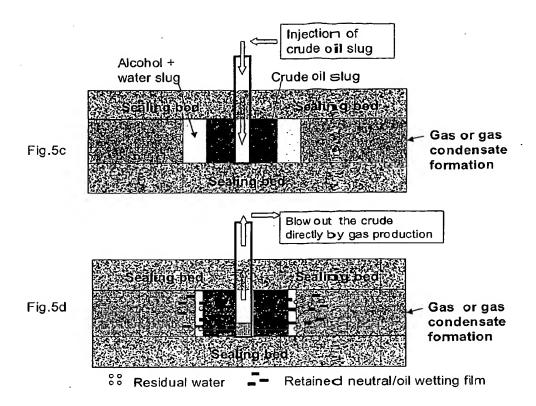


Fig. 5 Method 2 of treatment for gas or gas cond ensate reservoir case





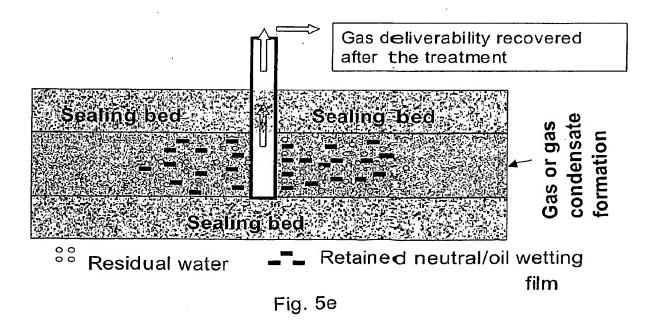
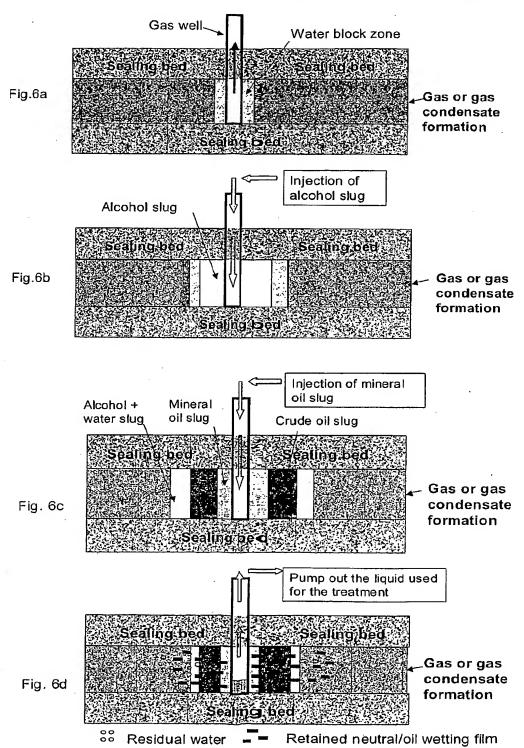


Fig. 6 Method 3 of treatment for gas or gas condensate reservoir case



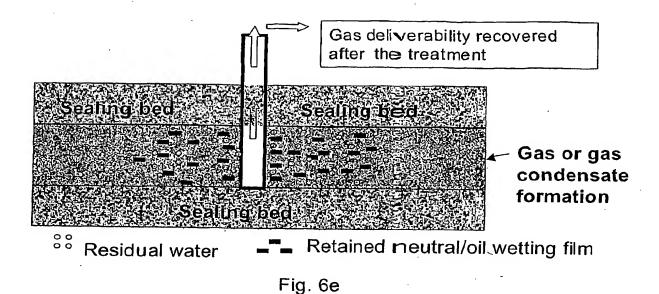


Fig. 7 Water coning case

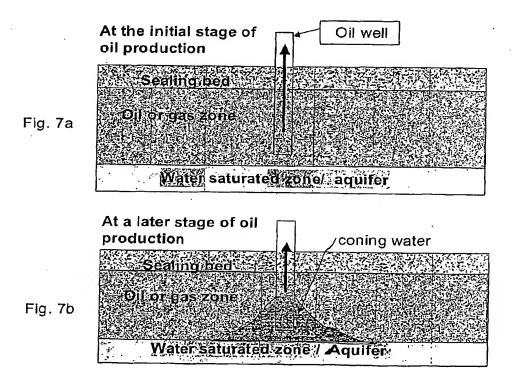
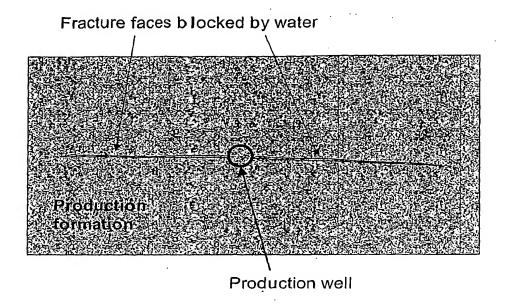
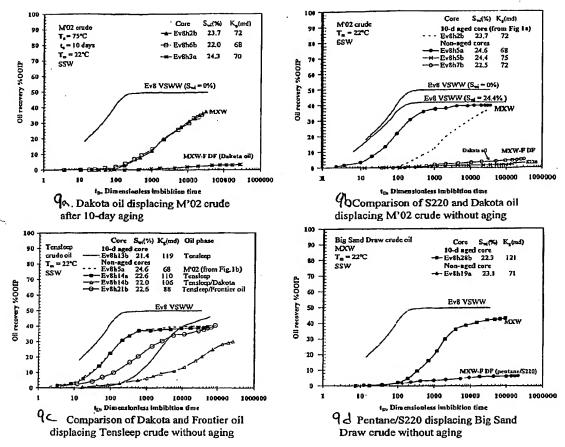


Fig. 8 Case with hydraulic fracture wells—plane view sketch





Wettability alteration was induced by displacement of crude oil with mineral oil or paraffinic oil directly.

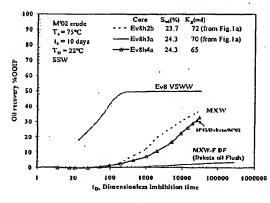


FIG. 10 Re-exposing surfaceprecipitated asphaltenes to fresh crude oil resulted in increased water wetness.

100000

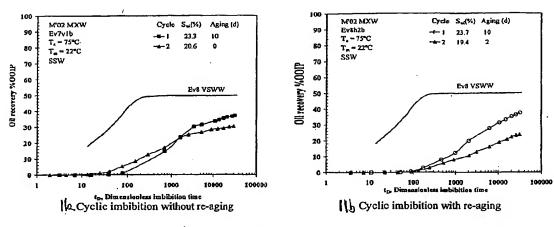
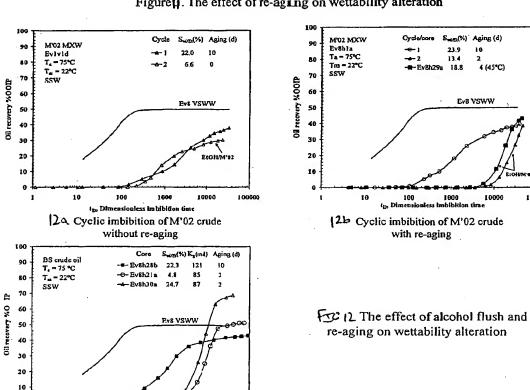


Figure . The effect of re-aging on wettability alteration

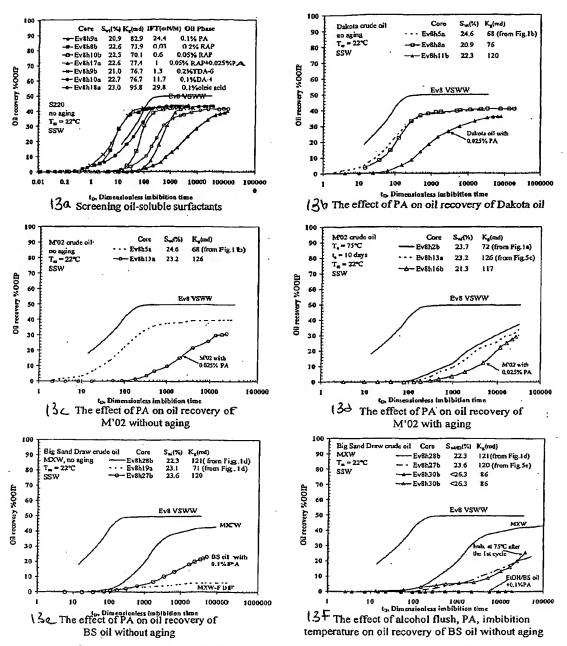


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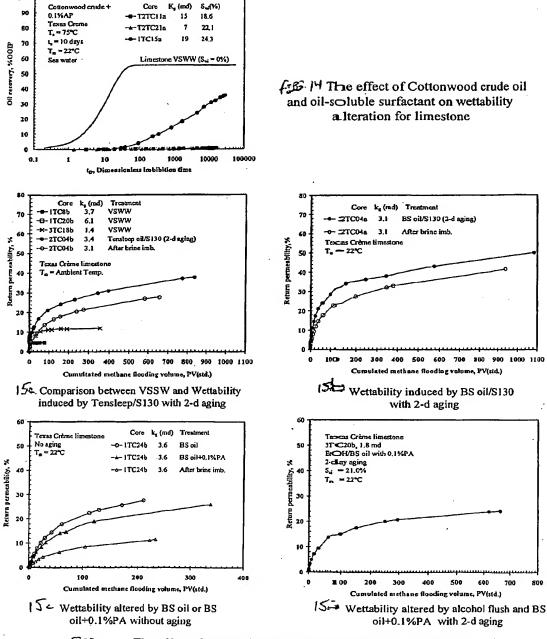
(2) Cyclic imbibition of BS crude with re-aging

1000

re-aging on wettability alteration



FST . 13 The effect of alcohol flush, oil-soluble surfactant and re-aging on wettability alteration for Berea sandstones



The effect of wettability alteration orn gas return permeability